Exploring Shear Thickening of Telechelic Associating Polymers through Stochastic Simulations

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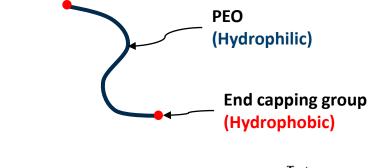


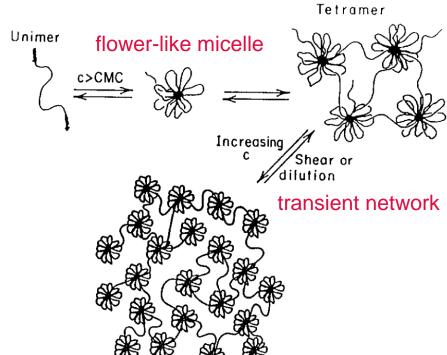






Telechelic Associating Polymers



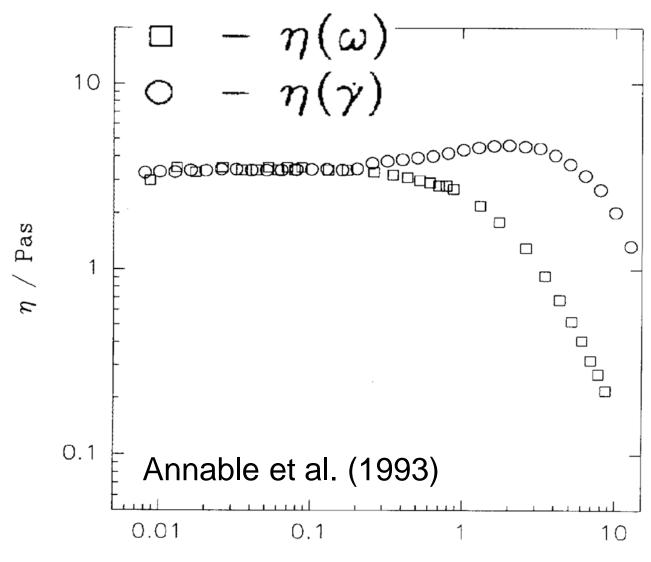


 10^2 Exp. data Suzuki et al. (2012) 10¹ 10^{0} 10⁻² T = 25, 20, 15, 10, 5 °C 10^{-3} 10^{-2} 10^{0} 10^{-1} 10^2 10¹ 10^3 $a_{\rm T}\omega/{\rm rad~s}^{-1}$

Xu et al. (1996)

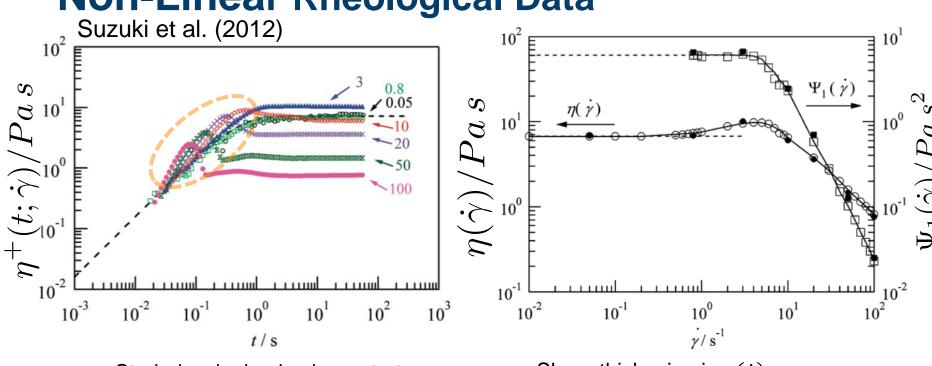


Steady Shear and Dynamic Viscosities





Non-Linear Rheological Data



Strain-hardening in shear startup

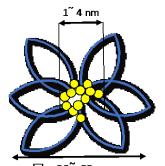
Shear thickening in $\eta(\dot{\gamma})$ **No** thickening for $\Psi_1(\dot{\gamma})$

Research Objectives

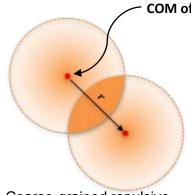
- 1. single Maxwell relaxation
- 2. breakdown of Cox-Merz Rule
- 3. strain-hardening in shear startup
- 4. shear thickening



Diffusion of Micelles with fixed network connectivity COM of micelle



□,,=20[~] 60 nm Simplified micelles with frictionless segments of chains



Coarse-grained repulsive interactions between micelles

Brownian force

$$\langle \boldsymbol{F}_{i}^{(Br)}(t)\boldsymbol{F}_{i}^{(Br)}(t')\rangle = 2k_{B}T\zeta_{i}\delta(t-t')\boldsymbol{I}$$

Repulsive interaction

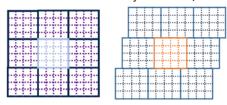
$$\mathbf{F}^{(rep)}(\mathbf{r}) = -C_{rep}k_BT \frac{D_m^2 - r^2}{D_m^3}\hat{\mathbf{r}}$$
 $C_{rep} = C_0p^k \Rightarrow C_{rep} = \langle C_0p^k \rangle$
(adjustable parameter)

 $au_m = rac{D_m^2}{k_B T/\ell}$ micelle diffusion time

Configurational Langevin equation:

$$\frac{1}{\zeta_k} \left(\frac{\partial \mathbf{r}_k}{\partial t} - \boldsymbol{\kappa} \cdot \mathbf{r}_k \right) = \sum_i \mathbf{F}_{ik}^{(rep)} + \sum_{i \in \mathscr{C}_k} \mathbf{F}_{ik}^{(el)} + \mathbf{F}_k^{(Br)}$$
 Fixed Connectivity

Lees Edwards boundary condition



 ζ_k : micelle friction coefficient of k-th micelle

 r_k : COM position vector of k-th micelle

 r_{ik} : relative vector between i-th and k-th micelles

 $\mathbf{F}_{ik} = \mathbf{F}(\mathbf{r}_{ik}) = F(r_{ik})\hat{\mathbf{r}}_{ik}$ κ : velocity gradient tensor Key parameters of micelle dynamics:

- repulsion coefficient (C_{rep})
- chain end-to-end distance/micelle diameter (R_c/D_m)
- maximally extendable chain length (FENE) (R_{max}/R_c)



Topological Rearrangement of Network (instant time)

Dissociation -----

$$P_{ij}^{dissoc} = \min\{1, \beta_{ij}\delta t\}$$

dissociation probability

$$\beta_{ij} = \beta_0 \exp\left(\frac{F^{(el)}(\mathbf{r}_{ij})l}{k_B T}\right)$$

Classical detachment frequency

Association -----

$$P_{ij}^{assoc} = \exp\left(-\frac{U(\mathbf{r}_{ij})}{k_B T}\right)$$

Boltzmann distribution
$$F_j(n) = rac{1}{Z_j} \sum_{i=1}^n P_{ij}^{assoc}$$

Normalized cumulated distribution function

F^{el}: force exerted on network strands between i-th and i-th micelles

 β_0 : thermal detachment frequency (= loop dissociation time)

 $\tau_0 = \beta_0^{-1}$: Loop dissociation time

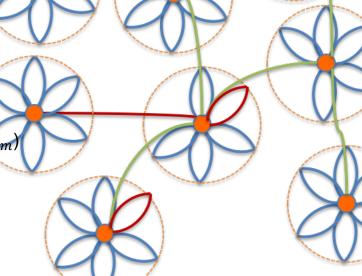
Key parameters for association/dissociation kinetics:

- Number of chains per micelles (N_c)
- length related to energy landscape of association (l/D_m)
- maximally extendable chain length (FENE) (R_{max}/R_c)
- Loop dissociation time / Brownian time (τ_0/τ_m)

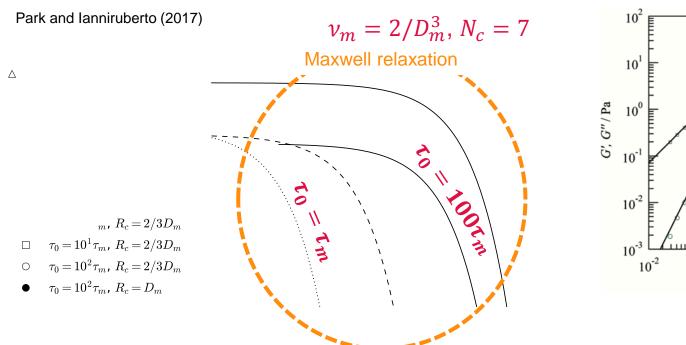
For details:

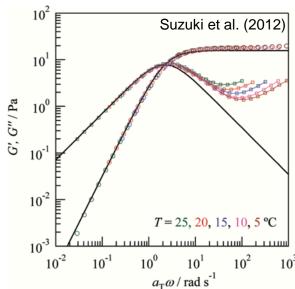
Park and Ianniruberto, J. Rheol. **61**, 1293 (2017)

Mitglied der Helmholtz-Gemeinschaft



Calculated Relaxation Modulus



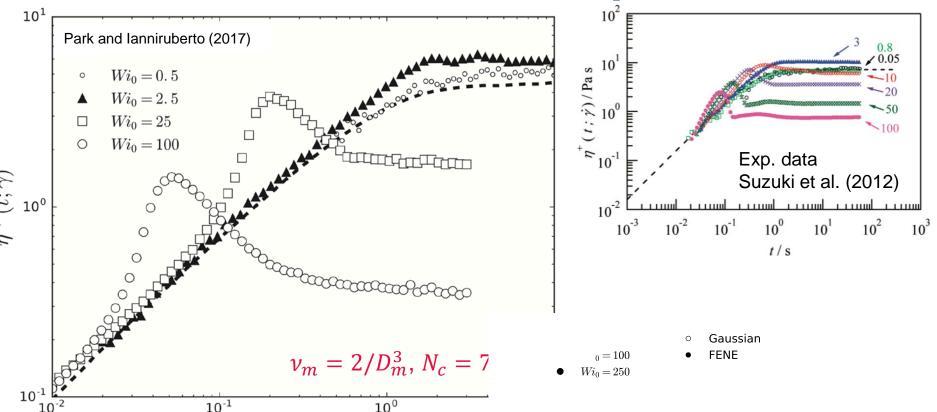


Symbols: calculated relaxation modulus (open: $R_c = 2/3D_m$, closed: $R_c = D_m$)

Lines: single Maxwell fit (characteristic times $0.75\tau_m$, $5.9\tau_m$, $62\tau_m$, and $105\tau_m$ from left to right)

- 1. System exhibit two steps of relaxation, the first relaxation due to repulsive Brownian motion while the latter one is network rearrangement.
- 2. The second relaxation can be described by single Maxwell model where the characteristic parameter is consistent with given loop dissociation times τ_0

Results of Shear Start-Up

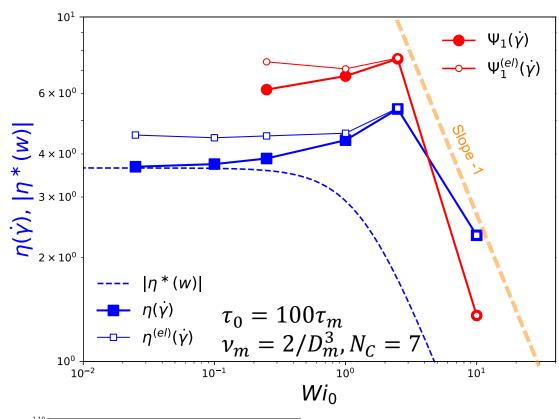


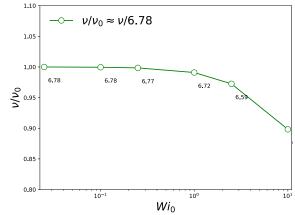
- time/ τ_0 1. Strain hardening is observed, and the stress growth function dominantly controlled by its elastic contribution.
- 2. No strain hardening is observed for Gaussian chain.

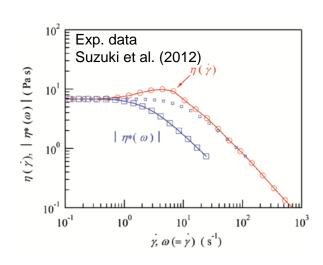
$$v_m = 0.1/D_m^3$$
, $N_c = 5$

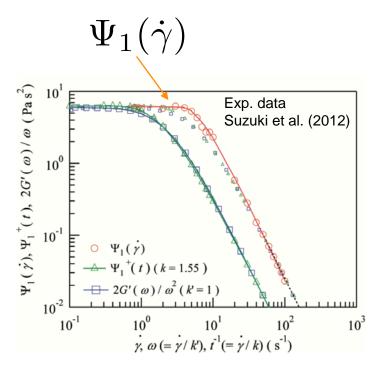
Park and lanniruberto (2017)

Results of Viscometric Functions









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Directional Contributions of Network Elasticity

$$\mathbf{T} = rac{1}{V_B} \sum_{i=1}^{N_m} \mathbf{R}_i \left(\sum_{j \in \mathbb{C}_i} \mathbf{F}_{ji}^{(el)} + \sum_j \mathbf{F}_{ji}^{(rep)}
ight)$$

$$\mathbf{T} = \mathbf{T}^{(el)} + \mathbf{T}^{(rep)}$$

$$\eta(\dot{\gamma}) = \frac{T_{xy}(\dot{\gamma})}{\dot{\gamma}}$$

$$\Psi_1(\dot{\gamma}) = \frac{T_{xx}(\dot{\gamma}) - T_{yy}(\dot{\gamma})}{\dot{\gamma}^2}$$

virial stress tensor

(el): network elasticity (rep): micelle repulsions

Need to understand directional contributions of network elasticity

$$\mathbf{T}^{(el)} = \nu \langle \mathbf{QF} \rangle = \nu \int f(\mathbf{Q}) \mathbf{QF}^{(el)}(\mathbf{Q}) d\mathbf{Q}$$
 where $\mathbf{F}^{(el)}(\mathbf{Q}) = \frac{\alpha_G}{1 - (Q/Q_{max})^2} \mathbf{Q}$

$$\mathbf{F}^{(el)}(\mathbf{Q}) = \frac{\alpha_G}{1 - (Q/Q_{max})^2} \mathbf{Q}$$

 $f(\mathbf{Q})$: PDF of elastically active bridges with bridge vector \mathbf{Q}

 $\Phi(\mathbf{Q})$: PDF of stress contribution of elastically active bridges

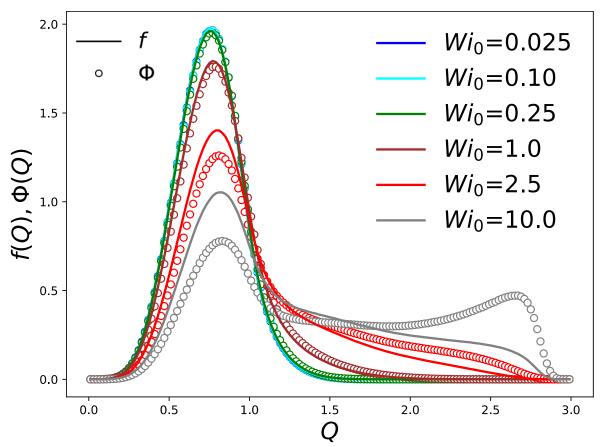
$$Z_{\Phi}\Phi(\mathbf{Q}) = \frac{f(\mathbf{Q})}{1 - (Q/Q_{max})^2} \quad \Rightarrow \quad \mathbf{T}^{(el)} = \underline{\alpha_G Z_{\Phi}\nu} \int \Phi(\mathbf{Q}) \mathbf{Q} \mathbf{Q} d\mathbf{Q}$$

 Z_{Φ} : normalization factor



Isotropic pre-factors

Bridge Length Distribution



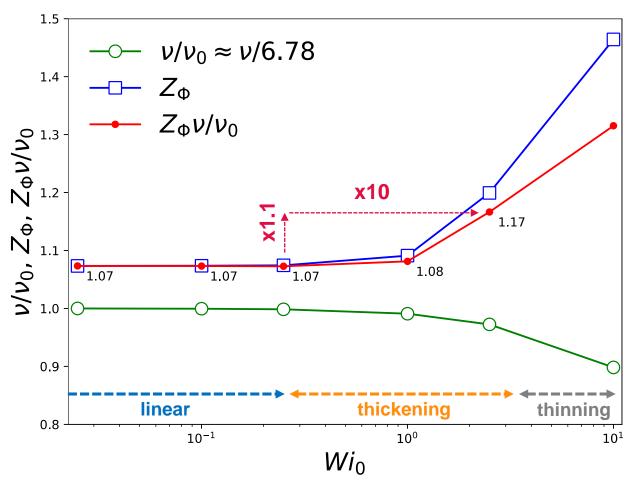
Linear

Shear thickening
Shear thinning

f(Q): PDF of elastically active bridges with $Q = |\mathbf{Q}|$

 $\Phi(Q)$: PDF of stress contribution of elastically active bridges with $Q = |\mathbf{Q}|$

Shear Rate Dependence of Isotropic Pre-factors

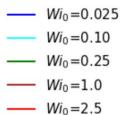


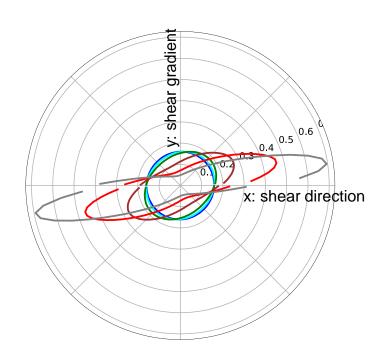
 $\nu(\dot{\gamma})$: Number density of elastically active bridges

 $Z_{\Phi}(\dot{\gamma})$: The isotropic contribution of finite extensibility

 νZ_{Φ} : A measure of isotropic contributions of network elasticity to stress tensor

Bridge Orientation Distribution



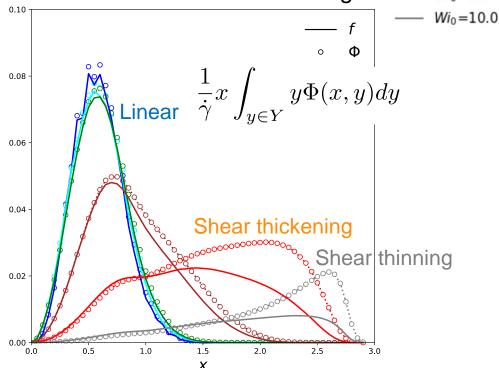


Orientation in shear (xy) plane

azimuthal angle

$$\phi \in [0, 2\pi)$$

shear stress distribution along x

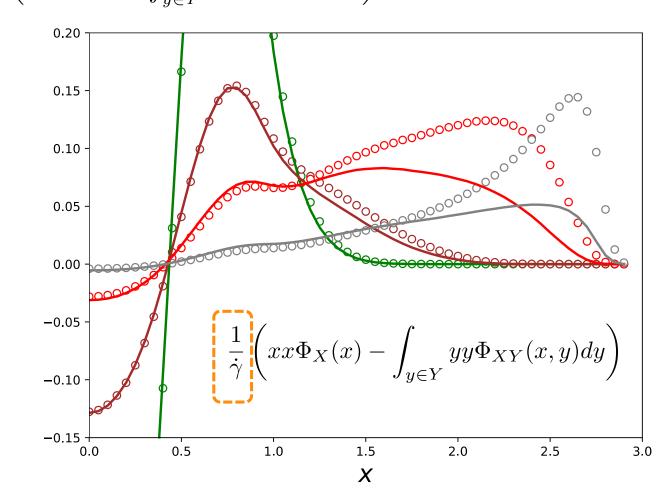


$$\eta^{(el)} = \frac{\alpha_G Z_{\Phi} \nu}{\dot{\gamma}} \int_{x \in X} x \left(\int_{y \in Y} y \Phi(x, y) dy \right) dx$$



Note: First Normal Stress Difference

$$\begin{split} \Psi_{1}^{(el)}(\dot{\gamma}) &= \frac{\alpha_{G} Z_{\Phi} \nu}{\dot{\gamma}^{2}} \left(T_{xx}^{(el)} - T_{yy}^{(el)} \right) \\ &= \frac{\alpha_{G} Z_{\Phi} \nu}{\dot{\gamma}^{2}} \int_{x \in X} \left(xx \Phi_{X}(x) - \int_{y \in Y} yy \Phi_{XY}(x, y) dy \right) dx \end{split}$$
 — Wi₀=0.25 — Wi₀=1.0 — Wi₀=10.0



 $Wi_0 = 0.025$

 $Wi_0 = 0.10$

Conclusion and Remarks

- Park and Ianniruberto (2017): a realistic simulation method reproducing (i) single Maxwell relaxation, (ii) strain hardening in shear start-up, (iii) deviation of Cox-Merz rule, and (iv) shear thickening.
- In this study, we produce non-linear rheological data for $\tau_0 = 100\tau_m$ with the same results for (i-iv).
- Two normalized PDF are introduced to decouple elastic stress tensor into isotropic and directional parts: bridge vector distribution, $f(\mathbf{Q})$, and elastic force distribution, $\Phi(\mathbf{Q})$.
- Effect of an isotropic pre-factors can be negligible for the both of shear thickening and thinning regimes.
- The orientation of network strands is the main reason of the transition from shear thickening to shear thinning in terms of steady shear viscosity.



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